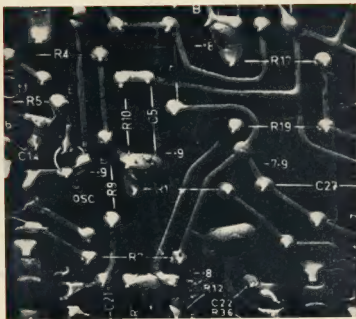


# AMATEUR RADIO

JANUARY 1964



Vol. 32, No. 1



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JANUARY 1964

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★

## OUR COVER

An enlarged portion of a printed  
circuit provides a modern style type  
of printing for our January edition.  
(Incidentally, all 1964 covers will be  
a red colour to differentiate between  
the 1963 (green) issues of "A.R.")

## FEDERAL COMMENT

★

The commencement of another year is the usual time chosen for looking  
to the future and injecting new ideas into an organisation such as ours.  
This year of 1964 promises to be no exception to the rule. However, a  
few comments of the previous Editorial are in order for it had not been  
confirmed at that time what the final results of the Extraordinary Confer-  
ence yielded. We are happy to confirm that the final Plenary meetings of  
the Conference, dealing with frequency extensions for the Space Services,  
preserved the status quo for the Amateur.

In Region 3, in which our particular interest lies, the Amateur band  
144-148 Mc. is exclusively Amateur, and in addition a footnote has been  
added to the effect that Amateurs may use artificial satellites for com-  
munication purposes in this part of the band between 144-146 Mc. Our  
delegation to the Conference, Mr. Tinkler, has now returned to Australia  
and submitted a verbal report to Executive on his trip. A written report  
will be published in this journal in the near future.

It is quite obvious from this report that the Amateurs would not have  
fared as well as they did had it not been for the preliminary work and  
exhausting discussions carried out by Amateurs with their administrations  
prior to and during the Conference. One most important point arising from  
this Conference appears to be the general feeling that future Conferences  
will follow the lines of this one, in that it seems unlikely that a full scale  
Conference such as the 1959 I.T.U. will continue in the future. They are  
more likely to take the form of Conferences dealing with particular Services  
such as the International Civil Aviation Organisation or Shipping.

This will mean shorter Conferences at more regular intervals because  
it has been recognised that a period of four to five months at a Conference  
is too long and too wearing on the nerves of the delegates. For this reason,  
the foresight of Federal Council in deciding to immediately start collecting  
funds was most timely. Some members have questioned the reasons for  
requiring so much money to be raised by Divisions. It is the opinion of  
Federal Council that a Fund must be set up in order to have representa-  
tion as and when required. We may not be so fortunate in the future  
as we have been in the past with our delegates who have had the backing  
of their companies in regard to salaries and expenses.

The Amateur has now grown in stature in international affairs, but  
in such growth must assume the responsibilities that it entails. He must  
now consider himself an important part of an international brotherhood  
which must be financially supported. It is certain that this subject will  
receive a great deal of attention at the next Convention, but it appears  
at this stage that an annual allotment from the membership subscription  
should be set aside in a fund for the Amateur Service. Call this a fighting  
fund if you wish, to protect our hobby, but despite its name, it should be  
raised in the interests of the Amateur Service as a whole. This in turn  
will mean greater co-operation between I.A.R.U. Societies, continual  
liaison to appreciate one another's problems and a greater sense of  
responsibility. This is the message then for the New Year—Let us all  
assume our proper responsibilities as members of the Amateur Service  
for a prosperous New Year.

FEDERAL EXECUTIVE, W.I.A.

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## A SINGLE SIDEBAND SYSTEM FOR 144 Mc.

J. F. BERWICK,\* VK3ALZ

IT has long appeared to the writer that the ideal band on which to demonstrate the superiority of side-band for weak signal work is 144 Mc. Although it may take a little time for receivers to improve to the stage where the full 9 db. gain is realisable, it is hoped that the device presented here will pave the way towards that goal.

Despite the imposing title, this is a comparatively elementary device consisting of three parts—

1. A transmitting up converter.
2. An AB1 driver stage.
3. A linear amplifier.

The design of such a converter calls for a little consideration. The problems are:—

- (a) Linearity of the s.b. amplifiers.
- (b) Spurious responses.
- (c) Stability of the oscillator.
- (d) Efficiency of mixer and amplifiers—an important consideration at 144 Mc.

It will be convenient to consider (a) and (d) in conjunction.

It transpires that some tube types which are highly suitable for mixer and amplifier service at h.f. on the grounds of linearity, are hopelessly inefficient at v.h.f.

The QE04/10 is a single ended beam tetrode on a B9G base and appears to be capable of good linearity and efficiency at 144 Mc.

### SPURIOUS RESPONSES

Any given frequency,  $f_x$ , can be generated by mixing any other pair of frequencies,  $f_x$  and  $f_y$ , according to the formula:—

$$Z = X \pm Y.$$

However, certain combinations of X and Y will simplify the problem of suppression of the spurious responses.

Suppose we wish to obtain 144 Mc. s.b. We have available s.b. at the following frequencies: 4 Mc., 14 Mc., 50 Mc. Which frequency to choose?

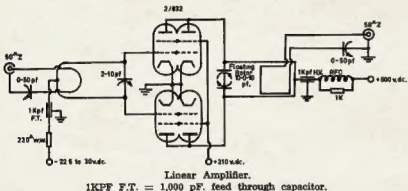
We have—

- (a)  $140 + 4 = 144$   
 $140 - 4 = 136$   
 (b)  $148 - 4 = 144$   
 $148 + 4 = 152$   
 (c)  $130 + 14 = 144$   
 $130 - 14 = 116$   
 (d)  $158 - 14 = 144$   
 $158 + 14 = 172$   
 (e)  $94 + 50 = 144$   
 $94 - 50 = 44$   
 (f)  $194 - 50 = 144$   
 $194 + 50 = 244$

**Clearly—**

- (a) and (b) are both unsatisfactory.
- (c) and (d) are both reasonably satisfactory.
- (c) is a quite popular scheme.
- (e) is highly satisfactory and is the scheme I have adopted.

(Continued on opposite page)

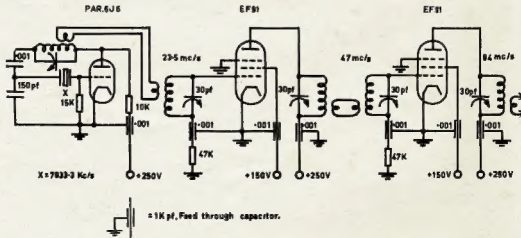


Clearly there is little reward in restricting the s.b. generator to a single band transmitter. One normally spends considerable time, not to mention expense, in developing an acceptable s.b. signal in the s.b. generator. It is highly desirable to use this acceptable signal on each band one normally operates. Hence the concept of the transmitting converter.

It is convenient, therefore, to investigate the linearity of tube types known to be efficient at 144 Mc.

It appears that certain deflection amplifiers have the desirable characteristics. Of these, the 12BY7 is probably the best. This tube is used extensively in commercial converters. I did not have this type available, but found the 6CK6 to be satisfactory. Of the other types used, the 5763 is satisfactory in Class A or AB1.

\* 107 Locksana Avenue, Glenroy, Vic.



Transmitting  
Converter,  
50 Mc. to 144 Mc.

Circuit continued  
on opposite page.

1KPF = 1,000 pF.  
feed through  
capacitor.

In this discussion it is assumed that both s.b. signal and the injection signal are free from spurious. The matter of spurious in the 50 Mc. transmitter was discussed in my previous article. An examination of the converter circuit will reveal that extensive measures have been adopted to eliminate spurious from the injection chain.

## STABILITY OF THE OSCILLATOR

This is determined from the equation  $x = 30 - \alpha$ , where  $x$  c.p.s. is the required stability of the injection chain oscillator, and  $\alpha$  c.p.s. is the overall stability of the s.b. source.

Since the practical aspects of oscillator stability have been adequately covered elsewhere and should be widely known, I do not propose to pursue this matter further.

## LINEAR AMPLIFIER

The choice of tubes is strictly limited at 144 Mc. I have settled for a pair of 832As—not because they are the ideal tubes to use, but because they were available and efficient, and will satisfy the power requirement. They can also be replaced at a later date by the better QCE06/40s, with very minor circuit changes. The amplifier is identical with my 50 Mc. linear except that the coils are replaced with lecher bars and the negative feedback loop is omitted.

## LINEARITY CHECKS

Despite what has been previously stated in this magazine and elsewhere, it appears that newcomers to s.b. (particularly the v.h.f. variety) imagine that a signal can be put on the air without any form of linearity check whatsoever. Any similarity between the resulting signal and s.b. can only be described as a remarkable coincidence.

Linearity checks are a must! If you don't have the necessary equipment to do the job, beg, buy or build it. The procedure for linearity checks is adequately covered in the Handbooks. ●

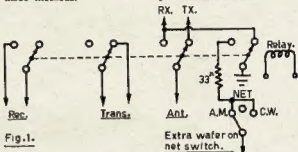
# PUSH-TO-TALK ON THE GELOSO G222TR TRANSMITTER

BILL MAGNUSSON,\* VK3AHT

THIS article will be of interest to all owners of the above transmitter. When operating in nets and contests one soon realises the shortcomings of a T/R switch that has to be reached for and rotated. I suppose the ultimate would be a foot operated switch and suspended mike or straight out vox. This article deals with p.t.t. but the problems encountered would be common to all three methods.

across the h.t. supply of the driver/sub-modulator. If this rotation is done fairly slowly the feedback and fade-away problem is eliminated, but if one is to use a relay here, circuit modifications must be made. That is unless you happen to have a relay with a wiping contact.

The net signal also tends to linger. This is because the net switch does not provide this bleed.



The rather complicated switching system dictates the use of some sort of relay control. A close inspection of the circuit reveals several problems, however, and discloses the reasons for some of the odd habits of this transmitter.

Most users will have noticed that when listening on your own frequency there is a tendency for the carrier to linger for some seconds after switching from transmit to receive. This is annoying and is due to the power supply not having any permanent bleeds. This has been overcome (to a degree) in the original circuit by using a wiping contact on the T/R switch which momentarily shorts a bleed resistor

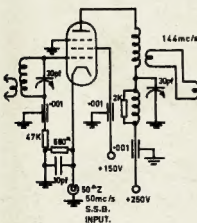
By using a four-pole double-throw relay to switch antenna and h.t., and by installing an extra wafer on the net switch, we can achieve very fast p.t.t. operation. The relay is wired as in the diagram so that section A controls the receiver, section B controls the transmitter h.t., section C controls the antenna change-over, and section D inserts the bleed resistor across the appropriate power supply.

Now due to the fact that this power supply is brought into action in the net position, provision must be made to remove this short at the same time. This is done by salvaging a switch wafer and longer shaft for the net switch. Mine came from a wrecked Geloso v.f.o. By an amount of gentle

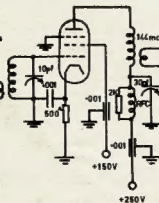
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\* 359 Williamstown Rd., Yarraville, Vic.

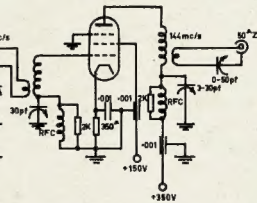
8CK6



5763-CLASS-A



QE04/10-CLASS-AB.1.





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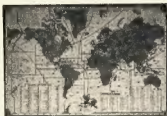
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# TRANSTRONIC PRODUCTS

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## S-METER, G.D.O., F/S. METER AND ABSORPTION WAVEMETER

W. H. FLETCHER, B.Sc. (G3NXT)

**M**EAURING instruments are an essential part of any Amateur's equipment, both to enable him to keep within the terms of his licence and to check on the effects of experimental adjustments to his equipment. Unfortunately, good meters are no longer as readily available or as cheap on the surplus market as they used to be, and the more the measuring units which can be designed to share one meter, the cheaper these instruments are to construct—the idea being, of course, to use one good meter movement for a variety of purposes.

### THE S-METER

The basic unit used at G3NXT consists of a valve-voltmeter type S-meter, as shown in Fig. 1. It is housed in a sloping-front meter case measuring 8" x 6" x 5" and is on the right in the picture. Its controls are, from left to right, the g.d.o. sensitivity control, S-meter sensitivity, and meter switch, which should preferably be a good quality ceramic item. The meter used

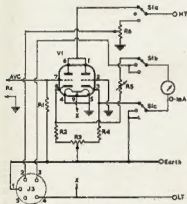


Fig. 1—Connections for the S-Meter Circuit, applicable to any Rx with the a.v.c. drive accessible. The 0-1 mA. meter movement is separately connected to the five-way socket J5, so that it can be picked up by an externally connected g.d.o. or absorption wavemeter.

in the prototype is 3° 0-1 mA. moving-coil but any 0-1 mA. or 0-500  $\mu$ A. meter with a clear scale is equally suitable.

The valve V1 is mounted on an L-shaped bracket fitted to the rear panel of the meter case by the bush of the balance potentiometer R3. The circuit is conventional, except that the sensitivity control R5 is placed in series with the meter, rather than using a potentiometer across the a.v.c. line. This arrangement protects the meter from overloading, whilst still giving a useful reading on weak signals.

The a.v.c. voltage can be derived from any convenient point on the receiver a.v.c. line. In the prototype it was

picked up from one of the inter-sectional coupling boards in the author's R107, and fed via screened cable to the front panel socket originally intended for the operator's lamp, having first removed and taped the lamp leads. A length of screened lead, fitted with wander plugs may then be used to connect the unit to the receiver.

With the CR-100, a.v.c. voltage is most conveniently derived from the a.v.c. line end of the resistor (marked R1 in the CR-100 manual) which feeds the first r.f. stage; this is located in a vertical position at the rear of the r.f. compartment.

### CIRCUIT ACTION

When a signal causes the receiver to develop an a.v.c. voltage, it is applied to g1 of the double triode V1. This reduces the current flowing through V1a and unbalances the bridge formed by the cathode resistors R2, 3 and 4, and the two sections of the double triode V1—causing a current to flow through the meter, which therefore gives an indication of relative signal strength.

To set up the S-meter, the meter switch S1 is set to the appropriate position and the receiver aerial terminal shorted to earth. The balance potentiometer R3 is adjusted to give a zero meter reading. Next connect an aerial to the receiver and tune in a strong local signal. The sensitivity control may be adjusted for full scale deflection (S9+). The author used his Top Band transmitter feeding a separate aerial for this adjustment. After a little experience the user will be able to interpret the deflection in terms of S-points.

Auxiliary units to make fuller use of the meter can be plugged into a five-pin Belling-Lee socket J3 mounted on the rear panel. H.t. and heater voltages are supplied as well as a direct connection to the meter. With the range switch in the centre position, the meter is connected directly to pins 1 and 3



The apparatus described by G3NXT in his article. The S-meter panel instrument is used also for the g.d.o. (left foreground), for which plug-in coils are used. The idea, basically, is to make the most of one really good panel instrument—in this case, a 3 in. 0-1 mA. moving-coil meter. The circuit shows how this is done.

and is available for measurements, in addition to the primary purpose of providing an absorption wavemeter.

### ABSORPTION WAVEMETER

The absorption wavemeter may be built into a small plastic, bakelite or paxolin box of similar dimensions to the case used for the grid oscillator.

(Continued on next page)

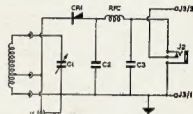


Fig. 2—Circuit of the Absorption Wavemeter using a diode rectifier. For panel meter indication, a plug connects to socket J3 in Fig. 1.

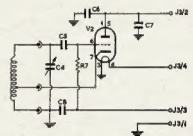


Fig. 3—The G.D.O. circuit used by G3NXT, with a 6C4. The unit derives its power and gives a meter indication by plugging it in as marked to J3 in Fig. 1. The sensitivity control for the g.d.o. is R6 in the Fig. 1 circuit.

Table of Values  
Fig. 1, 2, 3—S-Meter, G.D.O., and Absorption Wavemeter

- C1, C4—50 pF. var.
- C2, C3, C5, C7—0.001  $\mu$ F. ceramic.
- C6—100 pF. a.m.
- R1—4.7 megohms.
- R2, R4—500 ohms.
- R3—500-ohm bal. potentiometer.
- R5—10,000 ohms, 5-meter sensitivity.
- R6—100,000 ohms, 4w., g.d.o. sensitivity.
- R7—20,000 ohms.
- RFC—3.5 mH. r.f. choke.
- J1—Panel mounting coax socket.
- J2—Phone jack.
- J3—Five-way socket (see text).
- S1—3p. 3w. ceramic wafer.
- CR1—6AL5, or similar.
- V1—12AU6, ECC82, or similar.
- V2—6C4, L77, ECC6.

### COIL DATA

Wavemeter and G.D.O.					
Freq. Range (Mc.)	Turns	Enamel Wire	Diam.	Turns per Inch	Tap at
1.7-3.4	100	30g.	1"	c.w.	25
3.3-6.7	38	30g.	1"	c.w.	12
6.2-12	38	30g.	1"	c.w.	14
11.5-21	32	22g.	1"	c.w.	12
20-40	15	22g.	1"	16	5
38-84	4	22g.	1"	16	1 1/2

\* Reprinted from "The Short Wave Magazine," September 1963.

The same coils are used as with the g.d.o. They plug into a octal socket in the end of the box and are tuned by a 50 pF. air-spaced variable condenser mounted in the top of the box and fitted with an 180° scale; this can be directly calibrated.

The crystal diode CR1 is connected to the coil tap in order to obtain more efficient energy transfer between the high-impedance tuned circuit and the low impedance diode.

If a small aerial is plugged into J1, a standard coax socket, the unit will function as a Field Strength Indicator. And if a pair of high-impedance phones are plugged into J2, phone can be monitored.

For use as an Absorption Wavemeter, the unit is held with the coil near the tuned circuit under investigation and the 50 pF. variable condenser adjusted for maximum meter reading. The coupling should be kept to the minimum necessary to obtain a sharp reading, in order to minimise pulling between the two circuits.

If the instrument range switch is in the left hand position (see Fig. 1) a Grid Dip Oscillator may be plugged into the auxiliary socket.

#### GRID DIP OSCILLATOR

The Grid Dip Oscillator, shown on the left of the photograph uses a 6C4 in a Hartley circuit with plug-in coils.

The prototype was constructed in a 4" x 1½" x 1½" ex-A.M. pressed steel-case, but an Eddystone die-cast box would be more suitable.

The valve holder for the 6C4 is on an L-shaped bracket in the centre of the case, whilst an octal valve holder is mounted in the end of the case, to take the plug-in coils. The coils are wound on Denco ½" poly. octal plug-in formers for ranges 3-6. The coils for ranges 1-2 are on short lengths of 1" diameter paxolin tube glued into octal valve bases.

The tuned circuit is completed by a 50 pF. variable condenser mounted between the coil socket and the B7G valve holder. R.f. leads should be kept as short as possible for the v.h.f. range.

The sensitivity control R6, mounted on the main unit (see Fig. 1), controls the h.t. voltage to the oscillator. Some adjustment is necessary to compensate for variation of grid current with frequency, i.e. on change of band.

The g.d.o. will check the resonance of tuned circuits by noting the frequency at which a dip occurs in the grid current when the oscillator coil is coupled to an unknown circuit. It may also be used as a signal generator for testing receivers and converters. ●



"Well it looks a darned sight better without the call sign hovering above it."

## PROJECT OSCAR

This is directed to all u.h.f. groups, club leaders, s.w.l.'s and the whole Amateur fraternity. Oscar III. will, it is hoped, go up in April 1964, so be in it.

Oscar III. will be a communications satellite, and some very good DX is expected from it, particularly on the u.h.f. bands. So chaps now is the time to organise in groups and be ready to report on it, and also to contact other Hams through it. It will have a power of some two and a half watts. Remembering that Oscar I. and II. had only 300 milliwatts, some 52 reports came from Australia and the islands. The top number of loggings made by any one Ham was 51. This was made by VK1VP, of Canberra. This is the sort of a report that is appreciated.

It is hoped that all States will select their State Co-ordinator now and go to it, letting all and sundry know about Oscar III. As news comes to hand, it will appear in this magazine, on W.I.A. broadcasts, and in the various Bulletins. There will, it is hoped, be a Oscar III. network set up on 80 metres. You will have had some information in your State by now, so get cracking.

A model of Oscar will be on display in the various States soon, when we have found a way to get it around and at the same time cared for. No damage must befall this model as it has a long way to get yet.

Well chaps not too much more at this stage, see you later. May I take this opportunity to extend to all a very merry Xmas and a happy New Year.

—VK2HO, Co-ordinator.

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VKEMS	36 391	VKQKW	4 311		
VKRRU	3 393	VKRWL	14 311		
VKJAB	45 390	VKJATN	38 304		
VKEMK	43 394	VKXHR	19 193		
VKJAH	51 277	VKJLZ	61 190		
VKAFJ	31 261	VKXRV	33 195		
Amendment:					
VK3TL 65 138					
C.W.					
Call No.	Cer. Cnt-ries	Call No.	Cer. Cnt-ries	Call No.	Cer. Cnt-ries
VK3KB	16 316	VK3AGH	71 233		
VK3CK	26 391	VK3RP	66 229		
VK4FJ	29 388	VK3ARK	66 229		
VK3GL	5 379	VK3RTI	15 226		
VK3NC	19 366	VK3SD	6 223		
VK3RU	18 256	VK3RX	23 230		
Amendment:					
VK3EO 2 309 VK3TL 78 149					
OPEN					
Call No.	Cer. Cnt-ries	Call No.	Cer. Cnt-ries	Call No.	Cer. Cnt-ries
VK3RU	5 303	VK3HG	3 298		
VK3ACK	6 300	VK3NC	17 299		
VK4FJ	33 395	VK3JA	43 253		
VK3MK	74 348	VK3HR	7 233		
VK3AGH	65 306	VK3SD	4 231		
VK3AH	78 280	VK3WL	45 225		
Amendment:					
VK3TL 85 182					



# MORE ABOUT CRYSTALS AND CRYSTAL FILTERS

ARIE BLES,\* VK2AVA

**E**ARLIER in 1963 I wrote some articles on FT241A low frequency crystals and high frequency filters using type FT243 crystals. In the course of several months of matching and adjusting crystals and filters, I have learned a few things worth mentioning.

## FT241A TYPE CRYSTALS

If you have tried to either edge-grind them or silver-plate them for raising or lowering their frequencies, and have had the bad luck to break one or two of the suspension or contact wires, do not despair and throw that little rock away! In nine out of ten cases you can still fix your crystal to filter or oscillate, provided the little solder dots in the centre of the silver electrodes are still in position.

All you need to do is to find two thin strips of material, brass or tin-plate, to make two 1" long clips and to solder these to the crystal holder's pins. The strips must be flat and parallel, close together to hold the crystal between them, only touching the crystal at the two solder dots with a little pressure. Your crystal will be active again!



## FT243 CRYSTALS

Most people do not possess the proper skill to grind these crystals for raising their frequencies. Etching with a saturated ammonium bi-fluoride solution is the easiest way. But if you need to shift the frequency more than say 100 kilocycles, you may already have a very transparent slab of crystal with extra smooth surfaces and the etching goes very slowly or stands almost still. Just heat your bi-fluoride solution to say 150 or more degrees (Fahrenheit), but do it in the open for the fluoride fumes are dangerous. The etching effect can thus be speeded up considerably.

What to do when you have gone too far in frequency? Well, if it is going to be a filter crystal, you can still lower the frequency as much as say 500 cycles by changing the pressure on the crystal electrodes in the holder, or by careful reduction of the little corners on the crystal electrodes, using a small honing stone.

If more frequency change is required it will be better to keep the crystal as an oscillator and use a different one for the filter.

More shift in frequency on active oscillator rocks can be achieved by weighting the crystal surfaces. Some use cold solder for that and rub it in. Personally, I prefer to use a soft pencil and rub a little carbon on the crystal. If you have applied too much (when the crystal stops oscillating, or if the frequency has been shifted too much) just wash the crystal in soap and water and start again.

Up to 1,500 to 2,000 cycles shift can sometimes be effected. I have never noticed that the frequency of a treated crystal drifted up again with time. Someone once said that he feared the carbon might be shedded again due to vibration of the crystal!

Of course one can also lower the frequency of a crystal as an oscillator

## HIGHER FREQUENCY FILTERS

As I was playing with crystals for third overtone oscillator use, I started to wonder whether an active overtone crystal would perhaps also filter on or near that overtone frequency. And it does!

I have made up practical sets of filter crystals on 11 Mc., having a comparable bandwidth and shape factor as the filter sets on half that frequency. There is more work involved and much to be done on this project. Overtone crystals act differently from fundamental frequency ones and more careful adjustment is needed. But it works, and this can be a first example of such use of crystals.

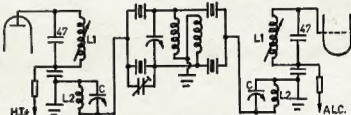


Fig. 1.

with a parallel capacity across it, but never expect more than 300 to 500 cycles shift in that manner. The crystal will stop oscillating with too much capacity across it.

## HYBRID CRYSTAL FILTER CIRCUIT

The impedance of the h.f. crystal filter circuit published in Feb. and August issues of "A.R." is low and either a cathode follower input stage is recommended or some provision must be made to limit the influence of this low impedance loading on the rest of the circuit. In any case, the signal magnitude across a low impedance device is always small.

I have not seen a comment or attempt to overcome this in any magazine, and the solution given in Fig. 1 may really be a novelty.

For 5.5 to 6.0 Mc. operation, the input and output transformers can be made of 1" diameter t.v.-type i.f. transformer forms. L1 is 45 turns, L2 is 15 turns, both close wound and only little spacing between the two coils. C is a 300/500 pF. mica compression trimmer. L1 is tuned to resonance with the former's iron slug, L2 with C, to give maximum output on the filter centre frequency.

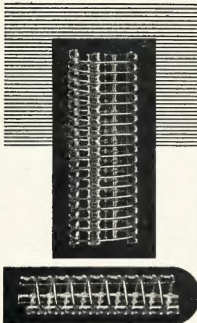
The effect is amazing, the better impedance match between the filter and the high impedances of the input and output sides gives an extra good flat-topped filter passband and loads of signal at the grid of the following stage.

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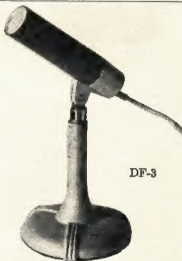
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## DIVISION OF 420-450 Mc. BAND

Editor "A.R.,"

Dear Sir,

With the eminent opening of the 420-450 Mc. band to Amateurs, the incentive to undertake some of the less common modes of transmission (particularly t.v. and f.m.) will be greatly increased. To try to cope with the problem of standard frequencies and channels to fit in with possibly existing equipment, I should like to submit the following for consideration by all Amateurs.

(1) The band 420-450 Mc. is wide enough to accommodate four channels, each 7 Mc. wide, for Amateur T.V., but to leave sufficient bandwidth for guard bands and other services, and to fit in with the standard domestic t.v. receiver which would most probably be the common method of reception only three channels are envisaged.

(2) In considering the domestic t.v. receiver (which would most probably be used as a tuneable i.f. to save modification) note must be taken that the use of the high band channels as the first i.f. would most likely add to the already difficult problem of converter noise at 420 Mc. and therefore the use of the low band is recommended. However, in the low band there are no three adjacent channels which would be the most convenient to use, but as channels 4 and 5 are adjacent, and channel 3 is spaced only 2 Mc. away, it would suggest the use of channels 3, 4 and 5 as the i.f., i.e. from 85 to 108 Mc., and this presupposes the use of a converter with local oscillator injection at 340 Mc.

Now to consider the placement of these bands within the 420-450 Mc. band. As has been seen on the majority of other v.h.f. bands, the majority of serious a.m., c.w. and s.s.b. operating is confined to the lower edges of the band, then it would seem logical to have the three t.v. channels at the top end of the band. Here though rises the problem of a guard band to reduce the possibility of out-of-band operation, and if consideration is given to the many possible d.s.b., i.e. non vestigial sideband transmissions which will most likely be undertaken, a minimum guard band of 2 Mc. is suggested.

This now leaves us with the following channelling:—

- (1) 420-425 Mc.—a.m., s.s.b., c.w.
- (2) 425-432 Mc.—a.t.v. ch. 1 (ch. 3 on t.v. rx).
- (3) 432-434 Mc.
- (4) 434-441 Mc.—a.t.v. ch. 2 (ch. 4 on t.v. rx).
- (5) 441-448 Mc.—a.t.v. ch. 3 (ch. 5 on t.v. rx).
- (6) 448-450 Mc.—guard band.

Now two further advantages immediately become obvious.

(a) Using a converter with 340 Mc. injection, the band 428-448 Mc. is converted to 88-108 Mc., i.e. the coverage of a standard f.m. v.h.f. receiver, many of which are still owned by Amateurs, and which are still available in many overseas equipments.

(b) The band 432-434 Mc. which lies between two t.v. channels is exactly three times 144.0 to 144.8 Mc., thus enabling the operators of many 2 metre transmitters to triple directly using existing transmitters and crystals. However, the first 5 Mc. has already been suggested for the more common modes, and therefore it is suggested that only 1 Mc. be available to these modes, e.g. from 432-433 Mc., the remainder from 433-434 Mc. being only for wide-band f.m. as this portion would be covered by the standard f.m. tuner.

In fact another point now arises. Many Amateurs when starting t.v. transmissions will not have the facilities for intercarrier sound, and then these two channels become eminently suitable for use as the accompanying sound channels for t.v. transmission without intercarrier sound. Intercarrier sound would normally be available through the standard t.v. receiver.

A further look at the Amateur t.v. position will show that many Amateurs wishing to commence video transmissions will wish to use double sideband

as being the easiest to generate. Therefore, to prevent any interference with any other services the a.t.v. ch. 3 of 441-448 Mc. could be used for double sideband, the unused or lower sideband then falling in the 434-441 Mc. of a.t.v. ch. 2 band. Therefore a.t.v. ch. 1, 425-432 Mc., should be reserved only for vestigial sideband transmissions with intercarrier sound as conforming to P.M.G. and C.C.I.R., and it is suggested that all official transmissions, e.g. W.I.A. etc., take place on this channel.

It is obvious that people wishing to do serious a.m., c.w. and s.s.b. work would build special narrow band converters to feed into their own communications receivers, but for persons wishing to experiment with t.v. the band resolves as follows:—

- (1) 420-425 Mc.—a.m., s.s.b., c.w., etc. (narrow band).
- (2) 425-432 Mc.—a.t.v. ch. 1, vestigial sideband, intercarrier sound, full C.C.I.R. specs. only.
- (3) 432-433 Mc.—a.m., sound associated with video transmissions in a.t.v. ch. 2 and 3, non-intercarrier.
- (4) 433-434 Mc.—wide band f.m., sound associated with video transmissions in a.t.v. chs. 2 and 3, non-intercarrier.
- (5) 434-441 Mc.—a.t.v. ch. 2, vestigial sideband only, intercarrier f.m. sound or non-intercarrier a.m. or f.m. as in (3) and (4).
- (6) 441-448 Mc.—a.t.v. ch. 3, vestigial or double sideband video, intercarrier f.m. sound or non-intercarrier a.m. or f.m. as in (3) and (4).
- (7) 448-450 Mc.—guard band to prevent out-of-band t.v. signals, but may be used for other narrow band modes if so desired.

These allocations are shown diagrammatically and will assist in an understanding. It would be most opportune if all Amateurs could consider these proposals and advise their local W.I.A. Divisions so that some form of gentleman's agreement may be formulated.

Incidentally, for those interested in building wide band converters with 340 Mc. injection as suggested, quartz crystals on 37.7778 Mc. (one-ninth of 340 Mc.) are being advertised in "Wireless World" by Henry's Radio at 7/6 sterling.

—Douglas W. Rickard, VK2ZDI.

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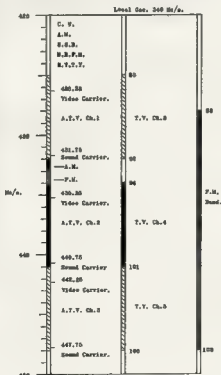
## PRINTED CIRCUITS FOR CARS

A British car manufacturer has announced that a new model car they will be producing will use a printed circuit wiring panel behind the dashboard. This will eliminate the familiar wiring harness with its multitude of leads.

★

## NOW REASONABLY WELL

Bill Barber, VK8DX, in a note to the Editor, sends his regards to all Amateurs and mentions that although he has not been in the best of health for the past two years, he is now reasonably well.



## A SIMPLE CONVERTER

WITH the advent of Y.R.C.'s I frequently hear demands for a simple converter. Such a converter has been described for a number of years in the A.R.R.L. Handbook. It is very inexpensive and can be used with practically any broadcast receiver, preferably those without a ferrite antenna stick system. The necessary power outlet could be fitted on a broadcast receiver under the supervision of the Y.R.C. leader and if necessary an aerial terminal.

Why is it inexpensive? The band-setting for 3.5 Mc. or 7.0 Mc. is by a two-gang capacitor about 865 pF. from any old scrapped radio. Band-tuning by 15 pF. capacitor (two for 7/9 advertised in "A.R."), one valve 6U8, one coil only (for the two bands, no switch). About a dozen resistors and condensers and, of course, the advantage that the bands are bandspread around 100° of the tuning dial.

For those who have not access to a A.R.R.L. Handbook, here is a brief description and circuit.

L1 couples aerial to L2. L2 and L3 form a bandpass circuit that can be tuned by the two gang (C1A and C1B) to 3.5 Mc. or 7.0 Mc. This bandpass circuit is coupled to the pentode section of the 6U8, acting as a mixer. In the anode circuit of the mixer is L6 and C7, tuned to 1700 kc., and L7 is coupled to the broadcast receiver.

L4, L5, C2 and C3, controlled from the panel, forms the main tuning. The oscillator tunes from 5.2 Mc. to 5.7 Mc. (Any Amateur would set this range for intending constructors.) Thus with this range the oscillator is 1700 kc. difference from the signal on 3.5-4.0 Mc. and 1700 kc. difference from 6.9 Mc. to 7.4 Mc. Thus which band appears as an i.f. of 1700 kc. will depend purely on the setting of the two-gang.

Note: The two-gang capacitor must be insulated from the chassis.

There are only two panel controls, a small knob on the two-gang termed "band set" and a slow motion device labelled "bandspread". If a slow motion

dial is not available, a cord drum from a scrapped radio driven by a rubber grommet on a  $\frac{1}{4}$ " shaft makes an ideal replacement. A cardboard scale can be glued to the drum and an old volume control with the wiper gear cut away makes a good panel mount for the grommet spindle. A s.a.c. answers any queries or assistance to constructors.

Coil data (all coils 1" diameter):

L1—8 turns 22 s.w.g.,  $\frac{1}{2}$ " long.

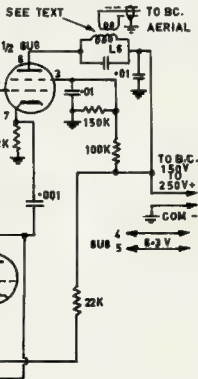
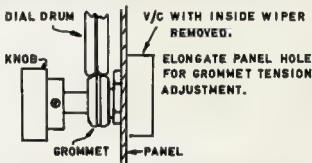
L2—19 turns 22 s.w.g., 19/32" long.

L3—Same as L2.

L4—21 turns 22 s.w.g., 21/32" long.

L5—8 turns 22 s.w.g.,  $\frac{1}{2}$ " long.

L1 is separated from L2 by 1/32" and wound on the same former. L4 and



L5 are separated by 1/32" and wound on same former.

Coils L1 and L2 should be mounted at right angles to L3.

The i.f. coils L6 and L7 can be a variety of arrangements:—

(1) 50-60 turns 28-32 s.w.g., paralleled with a 600 pF. capacitor and coupling winding of 20 turns wound on the cold end; 3/8" diameter slug tuned former.

(2) A r.f. choke of the all-wave type about 4 or 5 ples, and about 20 turns 28-32 s.w.g. wound near the cold end; no parallel capacitor with the choke.

(3) As for (2), but instead of a coupling winding, a 100 pF. condenser from the top or anode end to the b.c. set aerial terminal.

(4) The medium wave oscillator coil from a scrapped radio with a coupling winding of 20-30 turns added, or if a cathode tap of 100 pF. to b.c. set

Whichever course is adopted it must be fitted in a screened box or can, and of course to prevent b.c. break-through the whole should be in a metal box, a half size biscuit tin would make a good enclosure, or one of the aluminium or tin plate baking dishes sold in the multiple stores would do.

—A. F. W. Haddrell, VK3ZFC

(This circuit originally appeared in the A.R.R.L. Handbook.)

# AUSTRALIAN DX CENTURY CLUB AWARD

## OBJECTS

1. This Award was created in order to stimulate interest in working DX in Australia and to give successful applicants some tangible recognition of their achievements.
2. This Award, to be known as the "DX Century Club" Award, will be issued to any Australian Amateur who satisfies the following conditions.
3. A certificate of the Award will be issued to the applicants who show proof of having contacted one hundred countries, and will be endorsed as necessary, for contacts made using only one type of emission.

## REQUIREMENTS

1. Verifications are required from one hundred different countries as shown in the Official Countries List.
2. The Official Countries List will be published annually in "Amateur Radio" and will be amended from time to time as required. Should a country be deleted from the Countries List at any time, members and intending members will be credited with such country if the date of contact was before such deletion.
3. The commencing date for the Award is 1st January 1946. All contacts made on or after this date may be included.

## OPERATION

1. Contacts must be made in the H.V. Band Band 71 which extends from 3 to 30 Mc., but such contacts must only be made in the authorized Amateur Bands in Band 7.

2. All contacts must be two-way contacts on the same band. Cross band contacts will not be allowed.
3. Contacts may be made using any authorized type of emission for the band concerned.
4. Credit may only be claimed for contacts with stations using regularly assigned Government call signs for the country concerned.
5. Contacts made with ship or aircraft stations will not be allowed, but land-mobile stations may be claimed provided their specific location at the time of contact is clearly shown on the verification.
6. All stations must be contacted from the same call area by the applicant, although if the call sign is subsequently changed, contact will be allowed under the new call sign providing the applicant is still in the same call area.
7. All contacts must be made when operating in accordance with the Regulations laid down in the "Handbook for the Guidance of Operators of Amateur Wireless Stations" or its successor.

## VERIFICATIONS

1. It will be necessary for the applicant to produce verifications in the form of QSL cards or other written evidence showing that two-way contacts have taken place.
2. Each verification submitted must be exactly as received from the station contacted, and altered or forged verifications will be grounds for disqualification of the applicant.

3. Each verification submitted must show the date and time of contact, type of emission and frequency band used, the report and the location or address of the station at the time of contact.
4. A check list must accompany every application setting out the details for each claimed station in accordance with the details required in Rule 4.3.

## APPLICATIONS

1. Applications for membership shall be addressed to the Awards Officer, Box 2611W, G.P.O., Melbourne, Vic., accompanied by the verifications and the check list with sufficient postage enclosed for their return to the applicant, registration being included if desired.
2. A nominal charge of 2/6, which shall also be forwarded with the application, will be made for the issue of the certificate to successful applicants who are non-members of the Wireless Institute of Australia.
3. Successful applicants will be listed periodically in "Amateur Radio". Members of the D.W.C. wishing to have their verified country totals, over and above the one hundred necessary for membership, listed will notify these totals to the Awards Officer.
4. In all cases of dispute, the decision of the Awards Officer and two members of the Federal Executive of the W.I.A. in the interpretation and application of these Rules shall be final and binding.
5. Notwithstanding anything to the contrary in these Rules, the Federal Council of the W.I.A. reserves the right to amend them when necessary.

# WORKED ALL VK CALL AREAS (W.A.VK.C.A.) AWARD

## OBJECTS

1. This Award, to be known as the W.A.VK.C.A. Award, is offered by the Wireless Institute of Australia as tangible evidence of the proficiency of overseas Amateurs in making contacts with the various call areas of the Commonwealth of Australia.
2. The Award may be claimed by any Amateur in the world who is a member of an affiliated Society of the I.A.R.U., but no Australian Amateur will be eligible.

## REQUIREMENTS

1. A handsome Certificate will be awarded to any applicant who makes contacts with Australian Amateur Stations in the areas shown in the attached Appendix. The number of contacts required in each area is also shown.
2. In the case of applications prior to 1st January, 1964, a total of three (3) confirmations will suffice for VK1 and VK2; thereafter one confirmation for Australian Capital Territory (VK1) will be necessary as shown in the Appendix.

## OPERATION

1. Contacts between overseas stations and Australian stations must have been made on or after the 1st January, 1946.
2. Contacts may be made using any authorized frequency band or type of emission permitted to Australian Amateurs, but cross band contacts will not be allowed.
3. No contacts made with ship or aircraft stations in Australian territories will be eligible, but land-mobile or portable stations may be contacted provided the location at the time of contact is shown on the confirmation.

## VERIFICATIONS

1. The applicant must submit documentary proof, in the form of QSL cards or other written evidence, confirming that two-way contacts have taken place. Such verifications must show the date and time of contact, type of emission and frequency used, signal reports and location (in the case of portable or land-mobile operation) of the stations contacted.
2. Verifications must be submitted exactly as received, and forged or altered evidence may result in the disqualification of the station concerned.
3. A list, in accordance with the details required in Rule 4.3, must be submitted with the application for the Award.

## APPLICATIONS

1. All claims for the W.A.VK.C.A. Award must be made by the submission of the confirmations (Rule 2.1 or 2.3), together with the list (Rule 4.3), direct to "Awards Manager," Box 2611W, G.P.O., Melbourne, Australia. Sufficient International Reply Coupons must be enclosed to cover return postage of the confirmations to the applicant.
2. Where a reciprocal agreement exists between the W.I.A. and the applicant's Society, the appointed officer of that Society will carry out the check, and if correct, will forward a written application for the Award on behalf of the applicant, together with the list (Rule 4.3).
3. Applications will be examined by the Awards Manager, who will arrange for the Award to be forwarded either direct or through the applicant's Society. The Awards Manager's decision on the application and interpretation of these Rules will be final and binding.

4. Notwithstanding anything in the Rules to the contrary, the Federal Council of the W.I.A. reserves the right to amend these Rules as necessary.

## APPENDIX

Territory	Call Area	QSLs Required
Australian Antarctic	VK0	1
Heard Island		
Macquarie Island		
Australian Capital Territory	VK1	1
Lord Howe Island	VK2	3
State of New South Wales		
State of Victoria	VK3	3
State of Queensland	VK4	3
Thursday Island		
Willis Island	VK5	3
State of South Australia		
State of Western Australia	VK6	3
Fidlers Island	VK7	3
King Island		
State of Tasmania	VK8	1
Northern Territory		
Admiralty Islands	VK9	1
Bougainville Island		
Christmas Island		
Cocos Islands		
Neauru		
New Britain		
New Guinea		
New Ireland	VK9	1
Norfolk Island		
Papua Territory		

Note. In Areas above, where more than one confirmation is required, contacts may be made with any or all of the Territories listed in brackets.



# AUSTRALIAN D.X.C.C. COUNTRIES LIST

	Phone	C.W.		Phone	C.W.
AC3		Sikkim	FK8		New Caledonia
AC4		Tibet	FL3		Fr. Somaliland
AC5		Bhutan	FM7		Martinique
AP		East Pakistan	FN (prior 1/11/54)		French India
AP		West Pakistan	FO8		Clipperton I.
BV (C3)		Formosa	FO8		Fr. Oceania
BY (C)		China	FP8		St. Pierre & Miq. Is.
C9		Manchuria	*FQ8		Fr. Equatorial Africa
CE		Chile	TL8 (fr. 13/8/60)		Cen. Afric. R.
CE9, KC4, LU-Z, VK0, VP8, ZL5		etc., Antarctica	TN8 (from 15/8/60)		Congo Rep.
CE0A		Easter I.	TR8 (from 17/8/60)		Gabon Rep.
CE0Z		J. Fernandez Arch.	TT8 (from 11/8/60)		Chad Rep.
CM, CO		Cuba	FR7 (from 25/6/60)		Glorioso I.
CN2 (prior 1/7/60)		Tangier	FR7 (from 25/6/60)		Juan de Nova and Europa Is.
CN2, 8, 9		Morocco	FR7		Reunion I.
CP		Bolivia	FR7		Tromelin Is.
CR4		Cape Verde Is.	FS7		Saint Martin
CR5		Portuguese Guinea	FU8, YJ1		New Hebrides
CR3		Principe, Sao Thome	FW8		Wallis & Futuna Is.
CR6		Angola	FY7		Fr. Guiana & Inini
CR7		Mozambique	G		England
CR8 (prior 1/1/62)		Goa	GC		Guernsey and Deps.
CR8		Port. Timor	GD		Jersey I.
CR9		Macao	GD		Isle of Man
CT1		Portugal	GI		Northern Ireland
CT2		Azores	GM		Scotland
CT3		Madeira Is.	GW		Wales
CX		Uruguay	HA		Hungary
DJ, DL, DM		Germany	HB		Switzerland
DU		Philippine Is.	HC		Ecuador
EA		Spain	HC8		Galapagos Is.
EA6		Balearic Is.	HE		Liechtenstein
EA8		Canary Is.	HH		Haiti
EA9		Iñal	HI		Dominican Rep.
EA9		Rio de Oro	HK		Colombia
EA9		Spanish Morocco	HK0		Arch. of San Andres and Providencia
EA0		Spanish Guinea	HK0		Bajo Nuevo
EI		Rep. of Ireland	HK0		Malpelo Is.
EL		Liberia	HL, HM, GN5		Korea
EP, EQ		Iran	HP		Panama
ET2 (prior 14/11/62)		Eritrea	HR		Honduras
ET2, 3		Ethiopia	HS		Thailand
F		France	HV		Vatican
FB8		A'dam & St. Paul Is.	HZ		Saudi Arabia
FB8		Kerguelen Is.	I1, IT1		Italy
FC		Corsica	I1 (prior 1/4/57)		Trieste
*FF8		French West Africa	I5 (prior 1/7/60)		It. Somaliland
TU2 (fr. 7/8/60)		Ivory Coast R.	IS1		Sardinia
TY2 (fr. 1/8/60)		Dahomey Rep.	JA, KA		Japan
TZ2 (from 20/6/60)		Mali Rep.	JT1		Mongolia
XT2 (from 5/8/60)		Voltaic Rep.	JY		Jordan
5U7 (from 3/8/60)		Niger Rep.	JZ0 (pr'r 1/5/63)		W. New Guinea
5T5 (from 20/6/60)		Mauritania	K, W		U.S.A.
6W8 (fr. 20/6/60)		Senegal Rep.	KAQ, KG6I		Bonin & Volcano Is.
FG7		Guadeloupe	KB6		Baker, Howland and Ann. Phoenix I. (Inc. Canton I)
FH8		Comoro Is.			
FI8 (pr'r 20/7/55)		Fr. Indo China			

\*Fr. West Africa and Fr. Equatorial Africa: Only contacts dated prior to when the particular area obtained separate listing (as shown) will count.

	Phone	C.W.		Phone	C.W.
KC4		Navassa I.	ST2		Sudan
KC6		Eastern Caroline Is.	SU		Egypt
KC6		Western Caroline Is.	SV		Crete
KG4		Guantanamo Bay	SV		Dodecanese
KG6		Guam	SV		Greece
KG6		Marcus I.	TA		Turkey
KG6		(Rota, Tinian, Saipan, etc.)	TF		Iceland
		Mariana Is.	TG		Guatemala
KH6		Hawaiian Is.	TI		Costa Rica
KH6		Kure I.	TI9		Cocos I.
KJ6		Johnston I.	TJ (FE8)		Cameroon Rep.
KL7		Alaska	TL, TN, TR, TT		(see after FQ6)
KM6		Midway Is.	TS (3V8)		Tunisia
KP4		Puerto Rico	TU, TY, TZ		(see after FF6)
KP6		Palmyra Group, Jarvis I.	UA1-6, UN1		Eur. R.S.F.S.R.
KR6		Ryukyu Is.	UA1		Franz Josef Land
KS4B		Serrana Bank and	UA2		Kaliningrad Region
		Roncador Cay	UA9, 0		Asiatic R.S.F.S.R.
KS4		Swan Is.	UA0 (prior 1/9/60)		Wrangel I.
KS6		American Samoa	UB5		Ukraine
KV4		Virgin Is.	UC3		White Russian S.S.R.
KW6		Wake I.	UD6		Azerbaijan
KX6		Marshall Is.	UF6		Georgia
KZ6		Canal Zone	UG6		Armenia
LA		Bouvet I.	UH8		Turkoman
LA		Jan Mayen	UI6		Uzbek
LA		Norway	UJ8		Tadzhik
LA		Svalbard	UL7		Kazakh
LU		Argentina	UM3		Kirghiz
LX		Luxembourg	UN1 (prior 1/7/60)		Kar-Fin.Rep.
LZ		Bulgaria	UO6		Moldavia
MP4		Bahrain	UP2		Lithuania
MP4		Qatar	UQ2		Latvia
MP4		Trucial Oman	UR2		Estonia
OA		Peru	VE, VO		Canada
OD6		Lebanon	VK		Australia
OE		Austria	VK2		Lord Howe Is.
OH		Finland	VK4		Willis Is.
OH0		Aland Is.	VK9		Christmas I.
OK		Czechoslovakia	VK9		Cocos Is.
ON4		Belgium	VK9		Nauru I.
OX, KG1		Greenland	VK9		Norfolk I.
OY		Faeroes	VK9		Papua Terr.
OZ		Denmark	VK9		Terr. of New Guinea
PA0, P11		Netherlands	VK0		Heard I.
PJ		Neth. West Indies	VK0		Macquarie I.
PJ2M		Sint Maarten	VO (prior 1/4/49)		Newf./Lab.
PK (from 1/5/63)		Indonesia	VP1		British Honduras
PK1, 2, 3 (prior 1/5/63)		Java	VP2 (prior 1/8/58)		Leeward Is.
PK4 (prior 1/5/63)		Sumatra	VP2		Anguilla
PK5 (prior 1/5/63)		Borneo	VP2		Antigua, Barbuda
PK6 (prior 1/5/63)		Celebes and	VP2		Br. Virgin Is.
		Molucca Is.	VP2		Montserrat
PX		Andorra	VP2		St. Kitts, Nevis
PY		Brazil	VP2 (prior 1/8/58)		Windw'd Is.
PY0		Fernando de Noronha	VP2		Dominica
PY0		Trindade & Martin Vaz Is.	VP2		Grenada & Deps.
PZ1		Netherlands Guiana	VP2		St. Lucia
SD1 (ZS7)		Swaziland	VP2		St. Vincent & Deps.
SL, SM		Sweden	VP3		British Guiana
SP		Poland	VP4		Trinidad & Tobago

† One contact with each group formerly known as "Leeward Is." and "Windward Is." dated prior to 1/6/58 may be credited, in which case no further credit as a separate listing, as from 1/6/58, will be given those particular islands.

	Phone	C.W.		Phone	C.W.
VP5		Cayman Is.	ZD3		Gambia
VP5		Turks & Caicos Is.	ZD4 (prior 5/3/57)		Gold Coast
VP6		Barbados			Togoland
VP7		Bahama Is.	ZD6		Nyasaland
VP8		Falkland Is.	ZD7		St. Helena
VP8, LU-Z		South Georgia	ZD8		Ascension Is.
VP8, LU-Z		South Orkney Is.	ZD9		Tristan da Cunha and
VP8, LU-Z		South Sandwich Is.			Gough I.
VP8, LU-Z, CE9		Sth. Shet. Is.	ZE		Southern Rhodesia
VP9		Bermuda Is.	ZK1		Cook Is.
VQ1		Zanzibar	ZK1		Manihiki Is.
VQ2		Northern Rhodesia	ZK2		Niue
VQ6 (prior 1/7/60)		Br. Somalil'd	ZL		Chatham Is.
VQ8		Cargados Carajos Shs.	ZL		New Zealand
VQ8		Chagos Is.	ZL1		Kermadec Is.
VQ8		Mauritius	ZL4		Auckland and Campbell Is.
VQ8		Rodriguez I.	ZM7		Tokelau
VQ9		Aldabra Is.	ZP		Paraguay
VQ9		Seychelles	ZS1, 2, 4, 5, 6		Rep. of S. Africa
VR1 (includ. Canton Is.)		British	ZS3		Prince Ed. and Marion I.
		Phoenix Is.	ZS3		South-West Africa
VR1		Gilbert & Ellice Is.	ZS7 (see SD1)		
		and Ocean I.	ZS8		Basutoland
VR2		Fiji Is.	ZS9		Bechuanaland
VR3		Fanning & Christmas Is.	3A		Monaco
VR4		Solomon Is.	3W8, XV3		Vietnam
VR5		Tonga Is.	4S7		Ceylon
VR6		Pitcairn I.	4W1		Yemen
VS1 (prior 16/9/63)		Singapore	4X4 (from 14/5/48)		Israel
VS1, 9M2 (from 16/9/63)		West	5A		Libya
		Malaysia	5B4		Cyprus
VS4, ZC5 (from 16/9/63)		East	5H3		Tanganyika
		Malaysia	5N2		Nigeria
VS4 (prior 16/9/63)		Sarawak	5R6		(Madagascar) Malagasy
VS5		Brunei	5T5 (see after FF8)		
VS6		Hong Kong	5U7 (see after FF8)		
VS9		Aden & Socotra	5V		Togo Rep.
VS9		Kamran Is.	5W1 (ZM6)		Samoa
VS9		Kuria Muria	5X5 (VQ5)		Uganda
VS9		Maldiva Is.	5Z4 (VQ4)		Kenya
VS9		Sultanate of Oman	6N5 (see HL)		
VU2		India	6O1, 6O2 (from 1/7/60)		
VU		Laccadive Is.			Somalia Rep.
VU, XF		Andaman & Nicobar Is.	6W8 (see after FF8)		
XE, XF		Mexico	6Y (VP6)		Jamaica
XE4		Revilla Ggedo	7G1 (from 1/10/58)		Rp. of Guinea
XT2 (see after FF8)			7X2 (FA)		Algeria
XW8		Lao	9A (MI)		San Marino
XZ2		Burma	9G1 (from 5/3/57)		Ghana
YA		Afghanistan	9K2		Kuwait
YI		Irak	9K3		Kuwait-Saudi Arabia N.Z.
YK		Syria	9L1 (ZD1)		Sierra Leone
YN, YN0		Nicaragua	9M2 (prior 16/9/63)		Malaya
YO		Roumania	9N1		Nepal
YS		Salvador	9Q5 (previously OQ5-0)		Rep. of
YU		Yugoslavia			The Congo
YV		Venezuela	9S4 (prior 1/4/57)		Saar
YV0		Aves I.	9U5 (from 1/7/60 to 30/5/62)		
ZA		Albania			Ruanda-Urundi
ZB1		Malta	9U5 (from 1/7/62)		Rwanda Rep.
ZB2		Gibraltar	9X5 (from 1/7/62)		Burundi
ZC5 (pr. 16/9/63)		Br. Nth. Borneo			Cambodia
ZC3		Palestine			

# JOHN MOYLE MEMORIAL NATIONAL FIELD DAY CONTEST, 1964

Saturday, 8th February, to Sunday, 9th February

## DATE

Saturday, 8th February, to Sunday, 9th February, 1964.

## DURATION

From 1600 hours E.A.S.T., 8th February, to 1600 hours E.A.S.T., 9th February, 1964.

## OBJECTS

The operators of Portable and Mobile Stations within all VK Call Areas will endeavour to contact other Portable/Mobile and Fixed Stations in Australian and Overseas Call Areas.

## RULES

1. There shall be five sections in the Contest:—

- Portable/Mobile Transmitting, Phone.
- Portable/Mobile Transmitting, C.W.
- Portable/Mobile Transmitting, Multiple Operators, Open only.
- Fixed Transmitting Stations working Portable/Mobile Stations, Open only.
- Reception of Portable/Mobile Stations.

2. All Australian Amateurs may take part. Mobile or Portable Stations shall be limited to an input of 25 watts to the final stage. This power shall be derived from a self-contained and fully portable source. A Portable/Mobile Station shall not be located within one mile radius from the home(s) of the operator(s), nor be situated in any occupied dwelling or building.

Portable/Mobile Stations may be moved from place to place during the Contest.

No apparatus shall be set up on the site earlier than 24 hours prior to the Contest.

All Amateur bands may be used, but no cross-band operating is permitted.

3. Amateurs may enter for either (a) or (b), or both, in the Portable/Mobile sections.

4. One contact per station for phone and one for c.w. per band is permitted.

5. Entrants must operate within the terms of their licences and in particular observe the regulations with regard to portable operation.

6. Serial numbers consisting of RS or RST report plus three figures commencing with 001 and increasing by one for each successive contact shall be exchanged.

6a. Entrants in Section (c) for Multiple Operator Stations can set up separate transmitters to work on different bands at the same time. All such units of a Multiple Operator Station must be located within an area that can be encompassed by a circle not greater than half a mile diameter.

For each transmitter of a Multiple Operator Station a separate log shall be kept with serial numbers starting from 001 and increasing by one for each successive contact. All logs of a Multiple Operator Station shall be submitted by the Operator under whose Call Sign the transmitters are working. No two transmitters of a Multiple Operator Station are permitted to operate on the same band at any time.

## 7. Scoring:—

### (a) Portable/Mobile Stations:

For contacts with Portable/Mobile Stations outside entrant's Call Area .....

15 points

For contacts with Portable/Mobile Stations within entrant's Call Area .....

10 points

For contacts with Fixed Stations outside the entrant's Call Area .....

5 points

For contacts with Fixed Stations within the entrant's Call Area .....

2 points

### (b) Fixed Stations:

For contacts with Portable/Mobile Stations outside entrant's Call Area .....

15 points

For contacts with Portable/Mobile Stations within entrant's Call Area .....

10 points

8. The following shall constitute Call Areas: VK1 and VK2 combined, VK3, VK4, VK5 and VK6 combined, VK6, VK7, VK9 and VK0.

9. All logs shall be set out under the following headings: Date/Time (E.A.S.T.), Band, Emission, Call Sign, RST/No. Sent, RST/No. Received, Points Claimed. Contacts must be listed in numerical order.

In addition, there shall be a front sheet showing the following information:—

Name ..... Address .....  
Call Sign ..... Section .....  
Call Sign of other operator(s) (if any) .....  
Location of Portable/Mobile Station .....  
From ..... hours to ..... hours  
From ..... hours to ..... hours

A brief description of equipment used, bands used and points claimed, followed by the declaration:

"I hereby certify that I have operated in accordance with the rules and spirit of the Contest."

Signed..... Date.....

10. The right is reserved to disqualify any entrant who, during the Contest, has not observed the Regulations and the Rules of this Contest or who has consistently departed from the accepted code of operating ethics.

11. The decision of the Federal Contest Committee of the Wireless Institute of Australia is final and no disputes will be entered into.

12. Certificates will be awarded to the highest scorer in each Call Area. Additional Certificates may be issued at the discretion of the F.C.C.

## 13. Return of Logs:—

All entries must be postmarked not later than the 8th March, 1964, and addressed to the—

Federal Contest Committee, W.I.A.,  
Box 638J, G.P.O.,  
Brisbane, Queensland.

## RECEIVING SECTION

14. This section is open to all Short Wave Listeners in VK Call Areas. The Rules shall be the same as for the Transmitting Stations. Logs shall take the same form as for Transmitting Stations, but will omit the serial number received.

Logs must show the Call Sign of the Station heard, the serial number sent by it, and the Call Sign of the Station being worked.

Only one lot of points can be claimed for any one contact between two stations, for example: VK2AA/P calling VK3XX/P and exchanging numbers. Points can be claimed only for VK2AA/P working VK3XX/P. No points can be claimed for VK3XX/P working VK2AA/P during this particular contest.

Scoring will be on the same basis as for Transmitting Stations. It will not be sufficient to log a station calling CQ. A station may be logged once only for phone and once for c.w. in each band.

Awards.—Certificates will be awarded to the highest scorer in each Call Area.

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the simple r.f. tuned circuits decreases. At 30 Mc., with an operating Q of 40 in each tuned circuit, the 6-db. response points with two tuned circuits would be 1.4 Mc. apart. Thus at this frequency there is very little choice between the band-pass characteristics of the usual two-tuned-circuit r.f. amplifier and mixer, or the band-passed system.

Let's see that in spite of the problems outlined above, we've decided to build that "dream receiver" with broad-band r.f. circuits, in the interests of simplified home construction. What can we do to minimise the problems? Cross-modulation is caused by two factors: lack of selectivity, and insufficient dynamic range in the r.f. amplifier and mixer stages. We have sacrificed front-end selectivity for broad-band r.f. circuits, but if we are able to find some tubes with a very low equivalent-noise resistance, we can use low antenna-coupled and r.f.-amplifier gain. This would have the same effect as increasing the dynamic range of the tubes, thereby allowing us to handle stronger undesired signal levels than previously. While the same approach applied to a dream receiver would also be outstanding for the performance of a fairly acceptable band-pass receiver could be built.

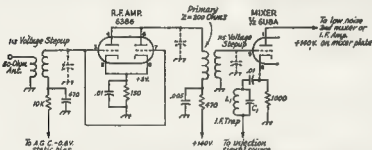


Fig. 2—Low-noise triode r.f. amplifier-mixer circuit with good cross-modulation characteristics. Resistors are  $\frac{1}{2}$  watt composition. LiCl is a trap circuit tuned to the i.f. output frequency of the mixer. See text for adjustment of interstage transformers.

Fig. 3 shows a rough schematic of such a front end. A 6386 removal-cutoff diode, with both sections in parallel, was selected for the r.f. amplifier. The plate load for the 6386 is very low, about 200 ohms. This keeps the voltage gain between the grid and plate less than unity, and no neutralization of the r.f. stage is necessary. Voltage gain to the mixer is obtained in the broad-band coupling transformer. A transformer voltage gain of 5, combined with a tube voltage gain of 0.8, provides an over-all r.f. stage gain of 4, which is adequate to overcome the mixer noise.

When setting up the transformer, adjust primary turns and coupling for a voltage gain of 0.8 from grid to plate of the 6386. Then re-check the secondary voltage to make sure there is a gain of 5 in the transformer.

The mixer is the triode half of a 6U8 or one section of a 12AT7, with cathode injection. These tubes used as mixers have an equivalent noise resistance of about 2,000 ohms, compared with 80,000 ohms in a pentagrid mixer such as a 6BA7. It is this low mixer noise resistance that allows us to use a total r.f. stage gain of only 4 and

still realise a 6.5 db. over-all noise figure. To accomplish similar sensitivity with the 6BA7 as a mixer would require an r.f. stage gain of nearly 25. This would result in severe degradation of mixer cross-modulation performance because of the very high levels of undesired signal that would appear at the mixer grid.

By using no more antenna-coil gain than is necessary to provide our 6.5 db noise figure, we keep undesired signal levels relatively low at the r.f. amplifier grid. The 6386 equivalent noise resistance under these operating conditions is 750 ohms, including the effect of first-mixer noise. An antenna-coil voltage gain of 5 will satisfy the noise-figure requirements.

The broad-band version of this front end has not been breadboarded to date. However, the tuned-version cross-modulation is shown in Fig. 2, curve A. A projected curve, C, based upon the gains and known cross-modulation levels in the tuned circuit, indicates the performance to be expected with broad-banding.

A word of caution is necessary concerning the injection signal for the triode mixer. To fully realise its low noise resistance, it is quite necessary to have a low-noise injection system as well as a source impedance of 50 ohms.

the output circuit, looking for the oscillator voltage to drop to one-half its unloaded value. The resistor value that causes this to happen is equal to the source impedance of the oscillator.

## THE TRANSISTOR FRONT END

Certainly a general article on receiver design these days should include a discussion of transistorised circuitry. Unfortunately, although it is fairly easy to obtain excellent sensitivity with the newest r.f. transistors, there is a severe limitation on strong-signal performance. In fact, unless a very severe reduction in sensitivity is accepted, a transistor front end may be expected to cross-modulate with 20 to 80 db. less undesired signal than an equivalent tube circuit. A typical transistor receiver cross-modulation curve is shown in curve E, Fig. 1.

Text books tell us that there is no significant difference in the noise figure of a given transistor in any of the three amplifier configurations: common base, common emitter, and common collector. This has been pretty well confirmed in practice as well as theory.

It is not possible to attain transistor noise figure of 4 db. as high in frequency as 290 Mc., with transistors in the three- to five-dollar class, thus making a 7-db. noise figure in the 3 to 30 Mc. range a relatively easy job. It should also be possible to design some excellent 6 and 2 metre portable equipment using these types. Some transistors that will do this job are the Philco types 2N1742, T2042, and T2028; Texas Instrument types 2N2186 and 2N2191, and the Amperex Universal type 2N2084.

In order to realise the best noise figure capabilities of an r.f. transistor, careful attention must be paid to both the recommended collector current for minimum noise figure and the recommended source impedance. The source impedance for minimum noise figure is generally near the value of the input impedance of the transistor in the common-emitter configuration. This impedance does not change significantly when the transistor is used in the other amplifier configurations. Fig. 5 shows how collector current and noise figure of the Philips 2N1742 are related.

Fig. 5 is a schematic of a typical common-emitter r.f. stage and mixer stage using the 2N1742 and 2N1743. The r.f. stage available power gain is partly a function of frequency, and varies from 45 db. at 3 Mc. to 35 db. at 30 Mc. A noise figure of 7 db. is attainable if the coil tap to the transistor is set to match the input impedance of the transistor. A collector current of 3.5 mA. corresponds to the recommended value for minimum noise figure, and is adjusted by selecting the

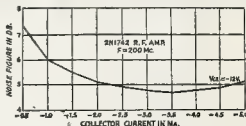


Fig. 4.—Typical curves of noise figure vs. collector current for a 2N1743 transistor as an r.f. amplifier, at 300 Mc.

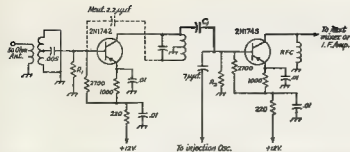


Fig. 5—Transistor r.f. amplifier and mixer circuit. Capacitances are in  $\mu\text{F}$ , except as indicated; resistances are in ohms, resistors are  $\frac{1}{2}$  watt. See text for adjustment of antenna coil tap. Interstage coil center-tapped.

C1—Selected for desired r.f. stage gain; typically 7 pF.

R1—Approximately 15,000 ohms; adjust for 3.5 mA. collector current.

R3—Approximately 15,000 ohms; adjust for 1.0 mA. collector current.

proper value for R1 (approximately 15,000 ohms).

Fig. 6 is a plot of input capacitance and input impedance vs. frequency, for various values of collector current, for the 2N1742. If the 2N1742 is used in the 3-30 Mc. frequency range, neutralization will probably not be necessary. However, if it is used at higher frequencies than 30 Mc., it would be desirable to add the network shown dotted in Fig. 6, to realize the maximum power gain and minimum noise figure.

#### CROSS-MODULATION IN TRANSISTOR R.F. STAGES

As stated previously, cross-modulation is a serious problem in transistorized receivers. R.f. transistors have an inherently limited dynamic range and will cross-modulate with some 20 to

when a strong local is wiping out the whole band.

A more exotic way of improving the r.f.-stage cross-modulation would be to improve the r.f. selectivity by using two or even three tuned circuits ahead of the r.f. transistor. Noise figure would suffer to a degree, but this is a compromise that the receiver designer is frequently required to make, even in a tube receiver.

Another means of improving the cross-modulation is to introduce degeneration in the emitter lead of a common-emitter r.f. stage. Caution must be exercised to assure that no more than 3 or 4 db. of degeneration is used, or the noise figure will deteriorate excessively. Other negative feedback schemes have been considered, but stability becomes a problem if any great amount of r.f. feedback is used.

#### TRANSISTOR MIXERS

A transistor used as a mixer will generally provide about 3 db. less gain than the same transistor operated as an r.f. amplifier. This is considerably different from tubes, where the conversion gain is approximately 25 per cent. of the tube's gain as an amplifier. R.f. gain in transistor front ends must be held to the minimum consistent with the desired noise figure, just as in a tube r.f. section; otherwise, mixer cross-modulation will become excessive.

A 10 to 12 db. mixer noise figure is fairly common for transistor mixers such as Philco 2N1743. In order to realize this noise figure, careful attention must be paid the recommended collector current and oscillator injection power requirements for the

particular transistor being used. Fig. 7 shows the effect of collector current on noise figure, and Fig. 8 shows oscillator injection power vs. mixer noise figure.

The formula for computing the effect of mixer noise figure on r.f. stage noise figure is

$$\text{Noise figure (power ratio) } F_{ab} =$$

$$F_a + \frac{F_b - 1}{A}$$

where  $F_{ab}$  is the total noise figure,  $F_a$  is the noise figure of the r.f. amplifier, and  $F_b$  is the noise figure of the mixer. These are expressed as power ratios. To get the noise figure in db., take 10 times the  $\log_{10}$  of the power ratio.  $A$  is the power-gain ratio of the r.f. stage including all coupling losses between stages. A numerical example is given below:

$$F_a = 4 \text{ db.; power ratio} = 2.5$$

$$F_b = 10 \text{ db.; power ratio} = 10$$

$$A = 10 \text{ db.; power ratio} = 10$$

$$\text{Therefore, } F_{ab} = 2.5 + \frac{10 - 1}{10}$$

$$= 2.5 + \frac{9}{10} = 3.4$$

$$10 \times \log_{10} 3.4 = 5.3$$

$$F_{ab} = 5.3 \text{ db.}$$

The noise figure (5.3 db.) is now referenced from the base of the r.f. amplifier transistor. Antenna-coupling circuit losses must also be considered in determining the over-all noise figure of the receiver. Although it is possible

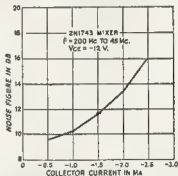


Fig. 8—Noise figure vs. collector current. 2N1743 as a mixer, 45 to 250 Mc.

to compute the over-all noise figure including the antenna-coil tuned-circuit losses, it becomes somewhat involved because three variables affect it. These are the losses inherent in the tuned circuit ( $Q$ ), losses due to mismatching, and the effect on transistor noise figure with change in source impedance. The computation of this is somewhat beyond the scope of this article. However, a good approximation may be made by setting the transistor tap on the input coil to match the input impedance of the transistor, measuring noise figure, and then moving the tap as close to the ground end of the coil as you can get, while still maintaining a 7 db. noise figure. This will keep signal levels to the r.f. stages as low as possible, thereby minimizing cross-modulation.

Needless to say, it is very desirable to use as high a tuned-circuit coil  $Q$  (Continued on Page 21)

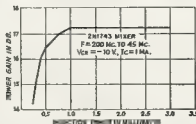


Fig. 7—Gain vs. oscillator injection power. 2N1743 as a mixer with  $V_{ce}$  equals -10 volts,  $I_c$  equals 1 mA. This curve applies over the frequency range 45-250 Mc.

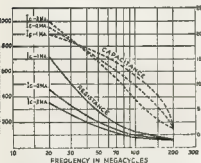
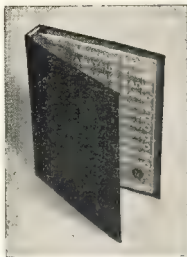


Fig. 6—Typical equivalent parallel input resistance and capacitance. 2N1742 with  $V_{ce}$  equals -10 volts, for selected values of collector current, output short-circuited.

30 db. less signal than a tube stage. Although to date no one has come up with a good answer to the problem, there are a few design tricks that help to minimize it.

The most simple device to minimize cross-modulation would be a 20-db. attenuator with a switch to connect it between the antenna and the receiver input stage when a strong off-channel signal is cross-modulating. Perhaps this sounds a bit agricultural, but it works, provided the desired signal is strong enough to overcome the 20-db. loss. Admittedly, this ruins the noise figure of the receiver, but there's not much point in having a 5 or 7 db. noise figure



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ADDRESS CORRESPONDENCE FOR THIS PAGE DIRECT TO THE SUB EDITOR

# H F S W L

## TYPE F1 EMISSION

Postmaster-General's Department

Treasury Place,  
Melbourne, C.2, Vic.  
13th Nov., 1963

Federal Secretary,  
Wireless Institute of Aust.,  
Box 2611W, Melbourne.

Dear Sir,

Further to our letter dated 26th July, 1963, in connection with type F1 emission in the Amateur Service (your letter of the 8th September refers), arrangements have now been made with effect forthwith to include type F1 emission, employing a maximum frequency shift of 850 c.p.s., in the types of emission permitted for use by the Amateur Service within all authorised frequency bands. The use of type F1 emission shall be confined to radio-teletype (R.T.T.Y.) systems employing a teleprinter type equipment using perforated tape or direct keyboard transmission and a printing mechanism for reception. The use of hand-speed Morse utilising type F1 emission is prohibited. R.T.T.Y. transmissions shall employ 3-unit code in accordance with International Alphabet No. 2.

For purposes of station identification in accordance with paragraphs 132 and 133 of the "Handbook for Operators of Radio Stations in the Amateur Service," July, 1963, which read—

"132. The operator of an Amateur Station shall transmit the call sign of the station being worked and the call sign allotted to the station that he is operating at the beginning and end of each session, and at least once in every five minutes during the session.

133. Call signs must, in all cases, be signalled in full and in such a manner as to leave no doubt as to their identity, and must include the nationality prefix letters 'VK'."

an Amateur Station licensee employing type F1 emission shall transmit call signs either by means of hand-speed Morse (type A1) or radio telephony (types A3 or F3) signals.

It is not proposed that the Department inform each Amateur Station licensee of the new condition at this stage, but it would be appreciated if you would be good enough to arrange for appropriate publicity through the Institute's Divisional Broadcasts and Magazine "Amateur Radio," please.

Yours faithfully,

(Sgd.) I. F. Pearson,  
for Director-General.

## NEW SOUTH WALES

During 1963 the VK3 Group showed a marked improvement on previous years. Attendances at the meetings were quite good. I feel sure that if more of our Group would come along they would enjoy what is offered and would certainly come again. Our thanks go to Phil Z2PI and Tim Z2TM for their continued support, and their patience in imparting knowledge which is a great inspiration to a.w.f.s. We are indeed fortunate in having two such stalwarts who are always there to help us on our way.

Our October meeting was a great success. Phil Z2PI gave an interesting talk on how to construct an all-band antenna and explained a three-translator converter for 2.8, 7 and 14 Mc. If any a.w.f.s. would like a copy of the above converter circuit, just drop me a line, plus a stamp and its yours.

Our Secretary still has a few copies of the AR7 manual on hand and members can purchase same for 10/6 plus postage. Write to Tom Harding, 33 Waratah St., Berowra, N.S.W.

We offer our congratulations to Ross L233Z/VK4 and to L263Z for their respective wins in the last N.P.D. Contest: good work lads.

Sid L233Z has his AMF300 going on all bands except 80 mhz at the moment. He sends word of logging OA, G and F2, which is not bad going on any rx. Sid is also having a go for his ticket and we wish him well.

Ross L233Z/VK4, who lives in the Rockhampton area, sends news of the prospects of a new rx, a GR30. He intends to use his 16RT for portable work and the other for his fixed station receiver.

Chas. L2311 reports that his 80 Mc. converter is not working, but Vince VK3VC has the matter under control.

Thought for the month: Use the right tool for the right job. T3, Chas. L2311.

## BY LADDER

	Countries Conf.	Hrd.	Zns. Conf.	S.a.b. Conf.	Hrd.	Wt. Stat.
E. Trebilcock	222	288	40	—	—	53
D. Granley	113	272	38	30	104	36
A. Westcott	93	159	31	9	107	11
M. Hilliard	83	235	33	39	165	18
M. Cox	80	226	29	39	168	12
P. Drew	66	198	27	29	121	14
C. Abernethy	56	96	30	—	—	—
N. Harrison	44	119	28	4	30	25
I. Thomas	43	128	30	16	97	14
G. Earl	35	121	22	30	104	3

## Wireless Institute of Australia

### Victorian Division

## A.O.C.P. CLASS

commences

MONDAY, 10th Feb., 1964

Theory is held on Monday evenings, and Morse and Regulations on Thursday evenings from 8 to 10 p.m.

Persons desirous of being enrolled should communicate with—

Secretary W.I.A., Victorian Division, P.O. Box 35, East Melbourne (Phone: 41-3535, 10 a.m. to 3 p.m.), or the Class Manager on either of the above evenings.

The DX has arrived on 6 metres and each State is working its share. Many new calls are appearing and some old ones are being used again. All States: VK1, 2, 3, 4, 5, 6, 7, 8, 9) are represented, so with just a fair share of luck and good conditions there should be no letdown in the 50 Mc. W.A.S. certificate awards.

VK2ZBV has been down south into VK3 on 29th Nov. A signal on 56.75 which could be 4ZGV has been heard a number of occasions in VK3 but no identification on the carrier.

JAs have been heard on at least three days during November in VK3. VK3ZKR scored JASYM on 24th. It was copying the JA but could not positively identify him at the same time worked him at 1400. Others heard JAs as early as 0630 same day.

Northern VK4s have also been amongst the JAs in recent weeks.

The band has been open from ZL to VK since 3rd. First in VK3 on 27th with ZL3 and almost daily until end of the month.

Numerous odd signals from VK5 and VK7 heard in VK3 during openings, but nothing worked to date. Nothing heard from VK5 direction to end of November.

The early closure of the notes leaves the page a little bare for this month. T3, ZGDP.

## QUEENSLAND

The v.h.f. meeting was held on Friday, 15th Nov., with about a dozen members present. At the meeting was the latest arrival on air, Roy VK4, who puts out a fine signal from Annerley. Also on the air is Ron 4ZBT who has recently returned from VK3. His portable frequency is 44.48 Mc. using 15w, to a 5753 and quarter wave length of hook-up wire. By the time you read this, he will have 5 elements beam in operation. At the time of writing these notes, Malcolm 4ZEL and Allan 4ZAW are mobile somewhere in VK3. George 4ZLG is mobile and will be going to VK3 at the end of November.

The summer DXZ is coming good with VKs 1, 2, 3, 5 and 7 being worked and a VK8 has been heard also.

Victor 4ZBT gave a lecture on Satellites to the monthly meeting of W.I.A. Several of the Brisbane boys are interested and will endeavour to track the satellite. T3, 4ZDF.

## WESTERN AUSTRALIA

Here in W.A. the coming of the summer months has meant a considerable rise in v.h.f. activity and as well as hearing a number of seldom-heard call signs on the air, a number of V.h.f. Group projects are also under way.

The 50 Mc. beacon tx which has been in operation at Cocos Is. for some time is being returned to Perth for an overhaul and it is planned to send it to Christmas Island where it will be operated by members of the Christmas Island Radio Club.

By the time that these notes are in print the new VK6VF beacon should be on the air and the details of operation are: Freq., 50.008 or 50.009 Mc. (depending on when the 50-Mc. band last closed); operation, virtually 24 hours a day; identification, call sign VK6VF keyed by using frequency shift keying (850 c.p.s. deviation); power, about 40 watts.

It is unfortunate that the new beacon was not ready for use sooner, but a considerable amount of work is entailed in building a beacon which is run continuously.

Incidentally ran for a total of about 20,000 hours, using the original output valve (an 807).

A number of 70 Mc. f.m. mobile transceivers have been purchased by the Institute for use in conjunction with the W.I.C.E.N. organisation in this State and these units are being modified for use on the 50 Mc. band. Small quantities of 70 Mc. a.m. mobile transceivers are also starting to become available, but it hasn't been decided how these will be used as yet.

One of the other points of interest is that Trevor 6ZDZ will be operating portable in Adelaide during the University vacation and no doubt those in VK3-band will know that he is around by this time. T3, 6ZDM.



# WORLD RANGE RECEIVERS — TRANSMITTERS — TRANSCEIVERS



## HALLICRAFTERS:

SR150 TRANSCEIVER  
SR160 TRANSCEIVER  
HT32B TRANSCEIVER  
HT44 TRANSMITTER  
HT45 LINEAR AMPLIFIER  
SX117 AMATEUR RECEIV'R  
SX122 GEN. COV. RECEIVER  
SX110 GEN. COV. RECEIVER  
SX118 GEN. COV. RECEIVER  
S108 GEN. COV. RECEIVER  
S120 GEN. COV. RECEIVER  
SX115 AMATEUR RECEIV'R  
XMITTER ACCESSORIES

## SWAN (Right):

SW240 VK TRIBAND  
TRANSCEIVER  
SW240 AC POW. SUPPLY  
SW12 DC POW. SUPPLY  
SW-VFO/TCU TRANS-  
CEIVER, VFO, VOX,  
SPK, CAL, and POWER  
SUPPLY.

## DRAKE (Below):

2B AMATEUR RECEIVER  
TR3 TRANSCEIVER  
ACCESSORIES by B. & W.  
W.R.L., HYGAIN, and  
BANDSPANNER.



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225 Victoria Road, Rydalmere — — — Phone 638-1713

### VIC.: ELECTRONIC SERVICES PTY. LTD.

10b Douglas Street, Noble Park — — — Phone 746-8446

### S.A.: TELEVISION & RADIOTRONICS

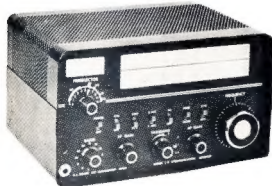
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### QLD.: GENERAL IMPORT DISTRIBUTORS

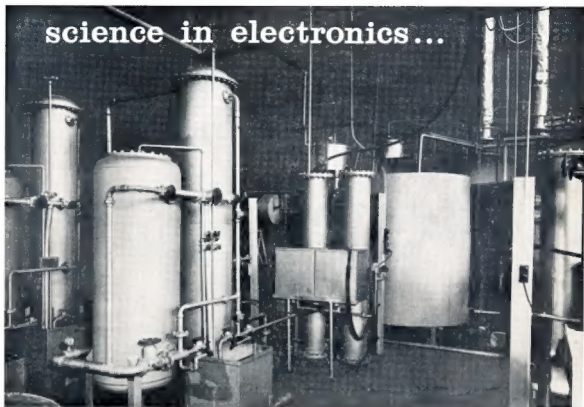
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AWV CONTINUOUS-TREATMENT WATER PURIFICATION PLANT

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Since tap-water contains sedimentary, organic and inorganic impurities it needs intensive purification before it can be used in an electronics factory, for example, for picture tube screen settling or in transistor manufacture.

A continuous-treatment water purification plant has been developed at A.W.V. in which initially chlorine is used to destroy slime-forming organisms and sediments are removed by coagulation and settling. The treated water is then passed through sand filters to remove suspended particles and through activated carbon filters to remove free chlorine. Inorganic salts are then eliminated by means of mixed-bed ion-exchange equipment.

The degree of purification obtained in the A.W.V. plant is such that the greatest metallic impurity is less than one part in ten million, total solids are less than one part in a million and the water is virtually an insulator—the resistance between opposite faces of a one centimetre cube is from five to ten megohms!



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